



# The optimal design of micro-punching die by using abductive and SA methods

**J.-Ch. Lin <sup>a</sup>, K.-S. Lee <sup>b</sup>, W.-S. Lin <sup>c,\*</sup>**

<sup>a</sup> Department of Mechanical Design Engineering, National Formosa University, 64 Wunhua Road, Huwei, Yunlin, Taiwan

<sup>b</sup> Department of Mechanical Engineering, Chien Kuo Technology University, Changhua, Taiwan

<sup>c</sup> Department of Mechanical and Computer-Aided Engineering, National Formosa University, 64 Wunhua Road, Huwei, Yunlin, Taiwan

\* Corresponding author: E-mail address: linwhs@nfu.edu.tw

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## ABSTRACT

**Purpose:** Punching process currently plays an important role in industrial mass production. The current study focuses on increasing accuracy, performance and extending service life of punches and dies. Optimizing the design of the punch and die has been a common topic for scholars.

**Design/methodology/approach:** The input parameters (punching times, clearance) and output results (wear) were used to construct a training database. The abductive network formulation established a relationship between input parameters and output results. By using the abductive modeling technique, the complicated and uncertain relationships between the input and output variables can be formulated into a useful mathematical model. Once the abductive network model was constructed, the relationships between input and output parameters variables became available. A simulated annealing algorithm (SA) with a performance index was established to optimize this process and find the best result as compared with the actual experiment values.

**Findings:** This study aims to establish the relationship between punching times, clearance and wear of micro punches using the abductive network, and to find relational model involving input parameters and output result of punching die in composite blanking processes. This model can be used to estimate wear between punch and die for industrial applications.

**Research limitations/implications:** Setting up the relational expression of punching times, clearance and wear requires a well-established database covering sufficient relevant parameters and data. In training the database, it is helpful to establish a good relational model among punching parameters. Incorrect data will cause abnormal wear. As a result, the mathematics model is difficult to converge and the neural network will inaccurately predict wear. In addition, the punching die may be changed prematurely, which increases production costs. Delay in replacing a worn punching die can result in poor quality of products.

**Originality/value:** As electronic production becomes increasingly smaller, the opportunity to use micro punches and dies will expand accordingly. This study established the relational expression of input and output, which can be used to correctly estimate any wear condition. This result is based on an abductive network and SA method.

**Keywords:** Optimal design; Composite; Experimental design; Abductive network; SA method

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## MANUFACTURING AND PROCESSING OF ENGINEERING MATERIALS

## 1. Introduction

Industrial progress has meant that punching dies used in mechanical applications is also used for mass production in the electronic/electric industry. The cross-applicability of punching dies arises because they conform with the product demand for 3C. With the development of Integrated Circuit (IC) processing technology, passive components are being increasingly miniaturized, ranging from early middle-chips to existing macro-chips. The increasing miniaturization of passive components leads to a requirement for smaller aperture of composite paper bags for various ICs. The accuracy of aperture for packaging bags, however, depends on the design of the punching dies. Good die design for punching can reduce the burr of the packaging bags. Hence, the punch and die can reach the accuracy required.

This study aims to identify the relationship between clearance and service life of micro punches using the Neural Network, and to find relational data involving the service life of punches and punching parameters in non-metal punching processes. The result can be used to estimate optimal clearance between punch and die for industrial applications.

In the past, the clearance between punch and die was generally set up for drawing process. [1,2,3,4,5,6] attempted to obtain the relationship between punch profile and die clearance via the optimization principle. Lieu and Sowerby [7], studied the best ways to obtain the parameters of optimal clearance and profile of punch and die during square drawing. Tai and Lin [8] also tried to obtain the optimal clearance value of punch and die during drawing process using the Neural Network and Simulated Annealing Method.

Luo [2] conducted experiments to obtain the optimal punching angle by using punches of different sizes during punching of round holes. Joo et al. [9] studied the micro-hole fabrication by mechanical punching process. Li et al. [10] studied the plastic stetus parameter and instantaneous clearance of a punching without burr. Cheung et al. [11], studied the relationship between IC packaged dam-bar and service life of punches. The clearance of punches and dies becomes smaller as a result of micro punching. This will adversely affect the accuracy of workpieces and reduce the service life of both punch and die components.

## 2. Experimental design

The experimental analysis used punches and dies made from high-speed steel subjected to surface grinding and heat treatment with hardness up to HRC 64. The punching machine was a 15t stand-up puncher, with a punching speed of 15 m/min. In conjunction with IC chips packaging, punch and die must be rectangular and right-angled ( $R \leq 0.03^R$  mm). They have a short side AO and long side BO as shown in Fig. 1. The shearing angle of the punch's cutting edge was  $12^\circ$ .

In order to explore the relationship between clearance and service life of the punch, eight groups of experimental data of side AO and side BO were established. The experimental data is listed in Table 1. Tables 2 through 5 show experimental values in millions of units punched for punch and die. This was training data allowing for an abductive network to set up the relationship between input data (clearance and punching times) and output result (wear).

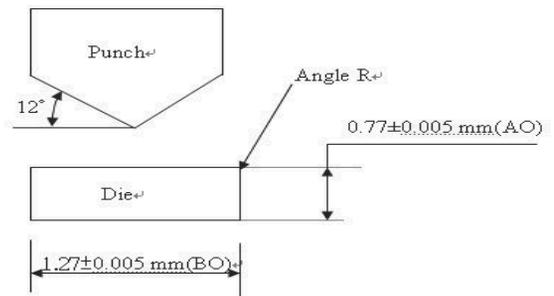


Fig. 1. Punch and die shap

The PET+PE+HMT composites were used for experiment. Where PET is Polyethylene Terephthalate, PE is Polyethylene, and HMT is one of Thermoset Dyed Polymer. The composition of experimental material is shown in Fig. 2. Fig. 3 and Fig. 4 show the wear condition of the punch and die after  $3 \times 10^6$  punching operation at a clearance of 0.015 mm.

Table 1.

The experimental data

Parameters	Level 1	Level 2	Level 3	Level 4
Punch/die AO-clearance	0.015mm	0.018mm	0.021mm	0.024mm
Punch/die BO-clearance	0.008mm	0.011mm	0.014mm	0.017mm

Table 2.

Punch AO-Side Wear Condition (mm)

Parameters	Clearance	Clearance	Clearance	Clearance
	0.015	0.018	0.021	0.024
Punching times				
$1.458 \times 10^6$	0.007	0.012	0.013	0.0132
$1.73 \times 10^6$	0.008	0.0125	0.014	0.02
$3.2 \times 10^6$	0.0175	0.0205	0.0220	0.025
$4.13 \times 10^6$	0.0235	0.028	0.031	0.034
$5.2 \times 10^6$	0.030	0.032	0.035	0.040
$6.27 \times 10^6$	0.0365	0.0375	0.040	0.047
$7.61 \times 10^6$	0.040	0.042	0.048	0.0525
$8.27 \times 10^6$	0.049	0.050	0.052	0.060

Table 3.

Punch BO-Side Wear Condition (mm)

Parameters	Clearance	Clearance	Clearance	Clearance
	0.015	0.018	0.021	0.024
Punching times				
$1.458 \times 10^6$	0.0095	0.001	0.008	0.010
$1.73 \times 10^6$	0.0195	0.015	0.0195	0.020
$3.2 \times 10^6$	0.0295	0.018	0.026	0.028
$4.13 \times 10^6$	0.031	0.021	0.029	0.031
$5.2 \times 10^6$	0.035	0.027	0.032	0.04
$6.27 \times 10^6$	0.0375	0.034	0.0395	0.0425
$7.61 \times 10^6$	0.044	0.035	0.041	0.0455
$8.27 \times 10^6$	0.045	0.0365	0.0470	0.0490

Table 4.  
Die AO-Side Wear Condition

Parameters	Clearance 0.015	Clearance 0.018	Clearance 0.021	Clearance 0.024
Punching times				
$1.458 \times 10^6$	0.7955	0.8015	0.8020	0.8070
$1.73 \times 10^6$	0.80	0.8075	0.8060	0.8075
$3.2 \times 10^6$	0.802	0.8080	0.8065	0.8082
$4.13 \times 10^6$	0.8075	0.8095	0.8070	0.8085
$5.2 \times 10^6$	0.8095	0.8096	0.8071	0.8086

Table 5.  
Die BO-Side Wear Condition

Parameters	Clearance 0.015	Clearance 0.018	Clearance 0.021	Clearance 0.024
Punching times				
$1.458 \times 10^6$	1.260	1.265	1.2550	1.2835
$1.73 \times 10^6$	1.2885	1.2900	1.2880	1.2910
$3.2 \times 10^6$	1.2910	1.2950	1.29	1.2945
$4.13 \times 10^6$	1.2910	1.305	1.2945	1.2950
$5.2 \times 10^6$	1.300	1.310	1.2950	1.3000

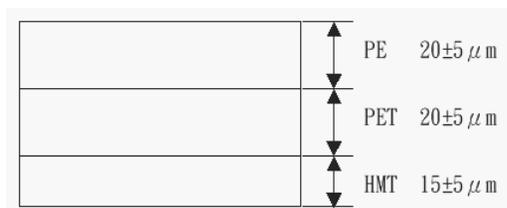


Fig. 2. The experimental composite



Fig. 3. The wear condition of the punch

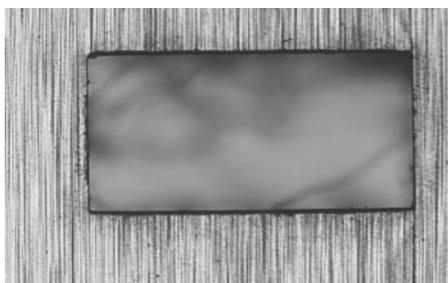


Fig. 4. The wear condition of a die

### 3. Image measurement

After a fixed number of punching times, the burr will be revealed just prior to the wearing out completely. When the burr size of the product exceeds the process standard of an IC factory, the production line is immediately shut down. The punching die is then taken apart to inspect its degree of wear. Companies producing passive components specify that the burr length of punched products shall be less than 0.03 mm. The punches must be replaced whenever the burr length exceeds 0.03 mm, indicating the end of service life.

#### 3.1. Image vision system

The burr can be examined by an image vision system as shown in Fig. 5, it includes the CCD (Teli 3910 CCD CAMERA), the image capturing card (National Instruments IMAQ PCI/PXI-1422) and the XY-Table. The image recognition software was programmed by using National Instruments Lab VIEW 6.i and IMAQ Vision Builder 6. This system can judge the size of burr automatically. Fig. 6 shows the burr of products.

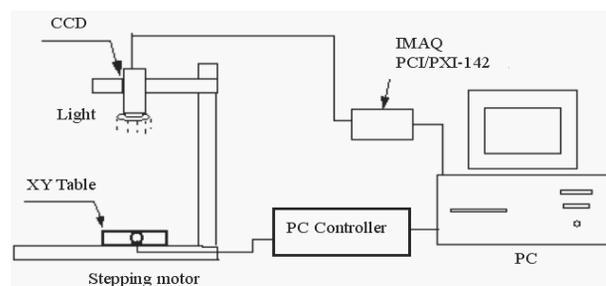


Fig. 5. Image vision system

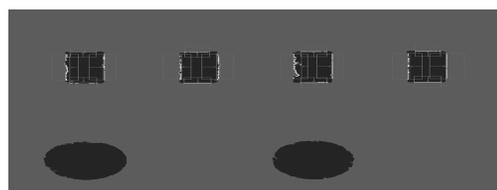


Fig. 6. Burr image of punched hole

#### 3.2. The contour searching method

Contour searching method was applied to find the border of parts by scanning, shown as Fig. 7. Each line searches the image contour to find the point on the edge, and connects each edge point to build the contour of the parts. From Fig. 8, each edge has a smooth change from bright to dark (or from dark to bright). This represents a smooth gray scale variation rather than a sharp change. The edge of the digital image is slightly blurred and the point position obtained by searching depends on the gray scale setting parameters. These parameters are: contrast; width of filtered wave; steepness; and relative width of search line.

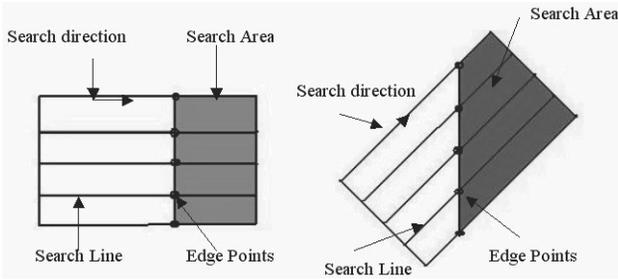


Fig. 7. Edge search

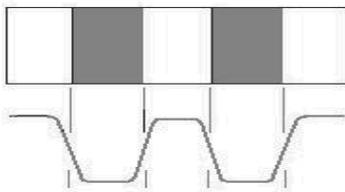


Fig. 8. Using gray scale measurement

### 3.3. Sub-pixel theorem

The minimum image unit is a pixel. The resolution of CCD was so poor that the measuring accuracy was low. The Sub-pixel technique was applied to divide one pixel into several pieces, using gray scale interpolation to obtain more precise pixel. This greatly increases the accuracy of an image, as shown in Fig. 9.

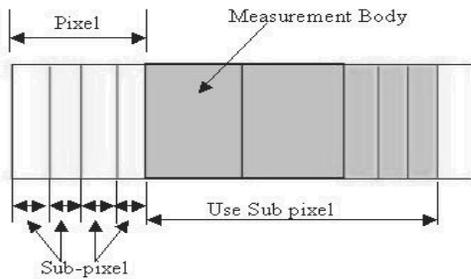


Fig. 9. Sub-pixel measurement

## 4. Abductive network synthesis and evaluation

Abductive network is a specific neural network. In an abductive network, a complex system can be decomposed into smaller, simpler subsystems grouped into several layers using polynomial function nodes. The polynomial network proposed by Ivakhnenko [12] is a group of methods of data handling (GMDH) techniques. These nodes evaluate the limited number of inputs by a polynomial function and generate an output to serve as an input to subsequent nodes of the next layer. The general polynomial

function in a polynomial functional node can be expressed as follows:

$$y_0 = B_0 + \sum_{i=1}^n B_i x_i + \sum_{i=1}^n \sum_{j=1}^n B_{ij} x_i x_j + \sum_{i=1}^n \sum_{j=1}^n \sum_{k=1}^n B_{ijk} x_i x_j x_k + \dots \quad (1)$$

where  $x_i, x_j, x_k$  are the inputs,  $y_0$  is the output, and  $B_0, B_i, B_{ij}, B_{ijk}$  are the coefficients of the polynomial functional nodes.

In this paper, several specific types of polynomial functional nodes are used in polynomial network to predict the residual blank length in some different kind of deep-drawing parameters. These polynomial functional nodes are named as normalizer (N), unitizer (U), white (W), singles (S), double (D) and triples (T) node. These are explained as follows:

### 4.1. Normalizer

A normalizer transforms the original input variables into a relatively common region.

$$a_1 = q_0 + q_1 x_1 \quad (2)$$

Where  $a_1$  is the normalized input,  $q_0$  and  $q_1$  are the coefficients of the normalizer, and  $x_1$  is the original input.

### 4.2. White node

A white node consists of the linear weight sums of all the outputs of the previous layer.

$$b_1 = r_0 + r_1 y_1 + r_2 y_2 + r_3 y_3 + \dots + r_n y_n \quad (3)$$

where  $y_1, y_2, y_3, y_n$  are the inputs of the node,  $b_1$  is the output of the node, and the  $r_0, r_1, r_2, r_3, \dots, r_n$  are the coefficients of the triple node.

### 4.3. Singles, double, and triples node

These are named according to the numbers of the input variables. The algebraic form of each of these nodes is shown in the following equation:

$$\text{single: } c_1 = s_0 + s_1 z_1 + s_2 z_1^2 + s_3 z_1^3 \quad (4)$$

$$\text{double: } d_1 = t_0 + (t_1 n_1 + t_2 n_1^2 + t_3 n_1^3) + (t_4 n_2 + t_5 n_2^2 + t_6 n_2^3) + (t_7 n_1 n_2) \quad (5)$$

$$\text{triple: } e_1 = u_0 + (u_1 o_1 + u_2 o_1^2 + u_3 o_1^3) + (u_4 o_2 + u_5 o_2^2 + u_6 o_2^3) + (u_7 o_3 + u_8 o_3^2 + u_9 o_3^3) + u_{10} o_1 o_2 + u_{11} o_2 o_3 + u_{12} o_1 o_3 + u_{13} o_1 o_2 o_3 \quad (6)$$

where:  $z_1, z_2, z_3, \dots, z_n, n_1, n_2, n_3, \dots, n_n, o_1, o_2, o_3, \dots, o_n$  are the inputs of the node,  $c_1, d_1$  and  $e_1$  are the outputs of the node, and the  $s_0, s_1, s_2, s_3, \dots, s_n, t_0, t_1, t_2, t_3, \dots, t_n, u_0, u_1, u_2, u_3, \dots, u_n$  are the coefficients of the single, double, and triple nodes.

These nodes are third-degree polynomial equations. The doubles node and triples node have cross-terms, allowing interaction among the node input variables.

### 4.4. Unitizer

On the other hand, a unitize converts the output to a real output.

$$f_1 = v_0 + v_1 i_1 \tag{7}$$

Where  $i_1$  is the output of the network,  $f_1$  is the real output, and  $v_0, v_1$  are the coefficients of the unitize.

To build a complete adductive network, the first requirement is to train the database. The information given by the input and output parameters must be sufficient. A predicted square error (PSE) criterion is then used to automatically determine an optimal structure. The principle of the PSE criterion is to select the least complex yet still accurate network as possible. The PSE is composed of two terms; that is:

$$PSE = FSE + K_p \tag{8}$$

Where FSE is the average square error of the network for fitting the training data and  $K_p$  is the complex penalty of the network, shown as the following equation:

$$K_p = CPM \frac{2 \sigma_p^2 K}{N} \tag{9}$$

Where CPM is the complex penalty multiplier,  $K$  is the number of coefficient in the network;  $N$  is the number of training data to be used and  $\sigma_p^2$  is a prior estimate of the model error variance.

## 5. Relationship between punch/die clearance and wear

Establishing the relationship of clearance, punching times and wear requires a well-established database covering sufficient relevant parameters and data. This database needs training to establish a good wearing model. Incorrect data and improper parameters, however, make it difficult to collect the wear information, while associated estimation leads to inaccuracy beyond control. These databases are listed in Tables 2 through 5. The punching times and wear condition of punch AO-side and BO-side are listed in Tables 2 through 3, and those of die AO-side and BO-side listed in Tables 4 through 5.

An adductive network synthesizes a three-layer network automatically. It is comprised of design factors (punching times and clearance size) and output factor (wear value). The polynomial equations used in this network are listed in Fig. 10 and Fig. 11. In the adductive network (Fig. 10), each layer of output had three sub-layers of input (e.g.,  $T_5$  (Triple5) had  $W_6$  (White6),  $S_7$  (Single7), and  $N_1$  (Normalizer1) three layers,  $T_4$  had  $T_5$  (Triple5),  $D_8$  (Double8) and  $W_6$  (White6) three layers. Input parameters include clearance of the punch/die and punching times. Output parameter includes the wear value of the punch's AO-side and BO-side. The others (die's AO-side and die's BO-side) individually have similar polynomial equations.

To verify the accuracy of the neural network, this study utilized another set of new dies for a wear test (see Table 6). The wear of punch AO side with clearance 0.015 mm et  $3 \times 10^6$  th punching times is 0.016 mm by actual experiment, while the neural prediction is 0.015 mm, with an error value of 6.3 %. The maximum error of the wear was on the die BO side with clearance

0.013 mm et  $5 \times 10^6$  th punching times, the wear prediction of the neural network is 1.2972 mm, and actual experiment value is 1.412 mm, with an error value of 8.1 %.

Table 6.

Comparison between the neural network prediction and experimental data

Method	The punch AO side		The punch BO side	
	wear with clearance $3 \times 10^6$ th	wear with clearance $8 \times 10^6$ th	wear with clearance $3 \times 10^6$ th	wear with clearance $8 \times 10^6$ th
Neutral prediction	0.015 mm	0.044 mm	0.026 mm	0.042 mm
Experimental data	0.016 mm	0.046mm	0.028mm	0.045 mm
Error	6.3%	4.3%	7.1%	6.7%

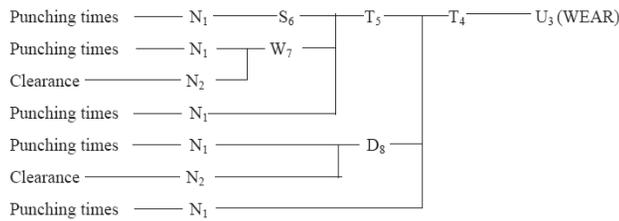
Method	The die AO side wear with clearance		The die BO side wear with clearance	
	$3 \times 10^6$ th	$5 \times 10^6$ th	$3 \times 10^6$ th	$5 \times 10^6$ th
Neutral prediction	0.796mm	0.810mm	1.290mm	1.297mm
Experimental data	0.821mm	0.842mm	1.402mm	1.412mm
Error	3.0%	3.8%	8.0%	8.1%

$N_1 = -1.94662 + 0.411243 * \text{Punching times};$   
 $N_2 = -5.72222 + 293.447 * \text{Clearance};$   
 $W_6 = 0.960326 * N_1 + 0.251905 * N_2;$   
 $S_7 = 0.0250502 + 0.891481 * N_1 - 0.0281086 * N_1^2 + 0.0440158 * N_1^3;$   
 $T_5 = 0.252064 + 0.986093 * W_6 - 8.11804 * S_7 + 7.15757 * N_1 + 0.602392 * W_6^2$   
 $- 3.18257 * S_7^2 - 8.4023 * N_1^2 - 1.73024 * W_6 * S_7 + 0.61861 * W_6 * N_1$   
 $+ 11.9775 * S_7 * N_1 - 1.0413 * W_6 * S_7 * N_1 + 0.353337 * W_6^3 + 1.18296 * S_7^3;$   
 $D_8 = -0.0119808 + 0.891481 * N_1 + 0.18949 * N_2 - 0.0281086 * N_1^2$   
 $+ 0.0382255 * N_2^2 + 0.0322999 * N_1 * N_2 + 0.0440158 * N_1^3 + 0.0392859 * N_2^3;$   
 $T_4 = 0.0393681 + 0.983441 * T_5 + 0.640928 * D_8 - 0.661664 * W_6 - 8.19017 * T_5^2$   
 $- 7.4301 * D_8^2 - 8.77204 * W_6^2 + 7.30834 * T_5 * D_8 + 9.29069 * T_5 * W_6$   
 $+ 7.79226 * D_8 * W_6 - 8.84366 * T_5 * D_8 * W_6 + 2.84633 * T_5^3 + 2.75418 * D_8^3$   
 $+ 3.24024 * W_6^3;$   
 $\text{Wear} = 0.0310312 + 0.0147681 * T_4;$

Punching times —  $N_1$  —  $W_6$  —  $T_5$  —  $T_4$  —  $U_3$  (WEAR)  
 Clearance —  $N_2$  —  $W_6$  —  $T_5$  —  $T_4$  —  $U_3$  (WEAR)  
 Punching times —  $N_1$  —  $S_7$  —  $T_5$  —  $T_4$  —  $U_3$  (WEAR)  
 Punching times —  $N_1$  —  $D_8$  —  $T_5$  —  $T_4$  —  $U_3$  (WEAR)  
 Clearance —  $N_2$  —  $D_8$  —  $T_5$  —  $T_4$  —  $U_3$  (WEAR)  
 Punching times —  $N_1$  —  $W_6$  —  $T_5$  —  $T_4$  —  $U_3$  (WEAR)  
 Clearance —  $N_2$  —  $W_6$  —  $T_5$  —  $T_4$  —  $U_3$  (WEAR)

(N: Normal node, W: White Node, S: Single Node, T: Triple Node,  
 PSE =  $8.6438 \times 10^{-7}$ , Punching times: Punching times  $\times 10^6$ )

Fig. 10. The relationship between punching parameters and wear of punch's AO-Side



(N: Normal node, W: White Node, S: Single Node, T: Triple Node, PSE=  $1.45 \times 10^{-6}$ ,  
 Punching times: Punching times $\times 10^6$ )  
 $N_1 = -1.94662 + 0.411243 * \text{Punching times}$ ;  
 $S_6 = 0.24844 + 0.558846 * N_1 - 0.26907 * N_1^2 + 0.246756 * N_1^3$ ;  
 $N_2 = -3.66809 + 293.447 * \text{Clearance}$ ;  
 $W_7 = 0.939094 * N_1 + 0.0501915 * N_2$ ;  
 $T_5 = -21.5951 + 88.2579 * S_6 + 2.4158 * W_7 - 51.2481 * N_1 - 4.64762 * S_6^2 + 41.3221 * W_7^2$   
 $+ 49.5672 * N_1^2 - 7.65221 * S_6 * W_7 + 14.9325 * S_6 * N_1 - 69.869 * W_7 * N_1$   
 $- 1.01751 * S_6 * W_7 * N_1 + 0.374606 * S_6^3 - 0.190928 * W_7^3 - 20.8571 * N_1^3$ ;  
 $D_8 = 0.147595 + 0.558846 * N_1 - 0.0133938 * N_2 - 0.26907 * N_1^2 + 0.104098 * N_2^2$   
 $+ 0.0319228 * N_1 * N_2 + 0.246756 * N_1^3 + 0.0400222 * N_2^3$ ;  
 $T_4 = 0.112132 + 0.044546 * T_5 - 0.337019 * D_8 + 0.882326 * N_1 + 1.76062 * T_5^2$   
 $+ 0.779504 * D_8^2 + 1.76557 * N_1^2 + 0.325588 * T_5 * D_8 - 3.56402 * T_5 * N_1$   
 $- 1.06171 * D_8 * N_1 - 2.30099 * T_5 * D_8 * N_1 + 0.962033 * T_5^3 + 0.899457 * D_8^3$   
 $+ 0.609214 * N_1^3$ ;  
 Wear =  $0.0312969 + 0.0125889 * T_4$ ;

Fig. 11. The relationship between punching parameters and wear of punch's BO-Side

### 6. SA method and optimal clearance selection

Metropolis et al. [13] proposed a criterion to simulate the cooling of a solid to a new state of energy balance. The basic criterion used by Metropolis is an optimization algorithm called "simulated annealing".

In this paper, the simulated annealing algorithm is conducted to search for the optimal clearance parameter. Fig. 12 shows the flow chart of the SA method. In the SA, initial temperature  $T_s$ , final temperature  $T_e$ , and a set of initial process parameter vectors  $O_x$  was given. The objective function  $obj$  is defined corresponding to the clearance values performance index. The objective function can be recalculated through all the different perturbed compensation parameters. If the new objective function becomes smaller, the perturbed process parameters are accepted as the new process parameters and the temperature drops a little in scale. That is:

$$T_{i+1} = T_i C_T \tag{10}$$

Where  $i$  is the index for the temperature decrement and the  $C_T$  is the decaying ratio for the temperature ( $C_T < 1$ ).

However, if the objective function becomes larger, the probability of acceptance of the perturbed process parameters is given as:

$$P_r(obj) = \exp \left[ \frac{\Delta obj}{k_B T} \right] \tag{11}$$

Where  $k_B$  is the Boltzmann constant and  $\Delta obj$  is the difference in the objective function. The procedure is repeated

until the temperature  $T$  approaches zero. It shows the energy dropping to the lowest state.

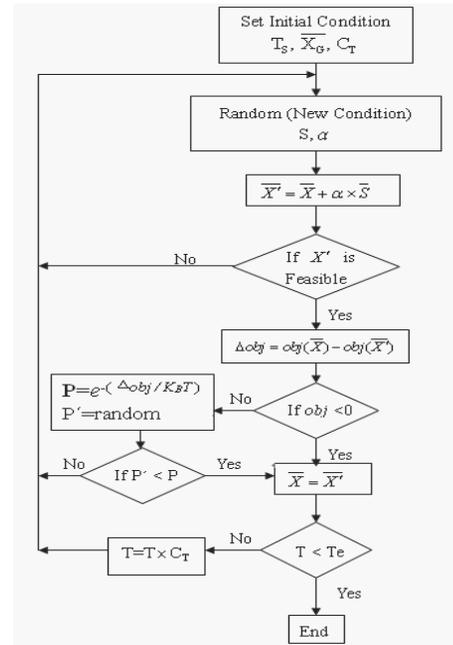


Fig. 12. The flow chart of SA method

Once the model of the relationship among the functions of the punching parameters (punching times, clearance) and punching die wear is established, this model can be used to find the optimal clearance to obtain the minimum wear. The optimal clearance values are obtained by using the objective function to serve as a starting point. The objective function  $Obj$  is formulated as flows:

$$Obj = w * (\text{Min. Wear}) (\text{punching parameters: clearance and punching times}) \tag{12}$$

where  $w$  is the weights function. In the meantime, the clearance values of the micro-punch should meet the simulation data method. In other words, the basic condition of optimization should fall in certain range, the clearance getting from optimization should be larger than the minimum clearance, and is smaller than the maximum clearance. The die punching times getting from optimization should be larger than the minimum punching times, and is smaller than the maximum punching times.

The inequality is given as follows:  
 The smallest clearance < clearance < the largest clearance (13)  
 The smallest punching times < punching times < the largest punching times (14)

The upper bound conditions should be kept at an acceptable level during the search routine to reach the optimization clearance design.

### 7. Results and discussion

This study explored the relationship of die clearance, the number of punched hole and wear, these parameters can estimate the service life of punching die. The experimental data using

punching process are shown in Figs 13 through 16. The punch short side (AO=0.77 mm) indicates that a punch's wear value is proportional to the clearance, and proportional to the punching times as shown in Fig. 13.

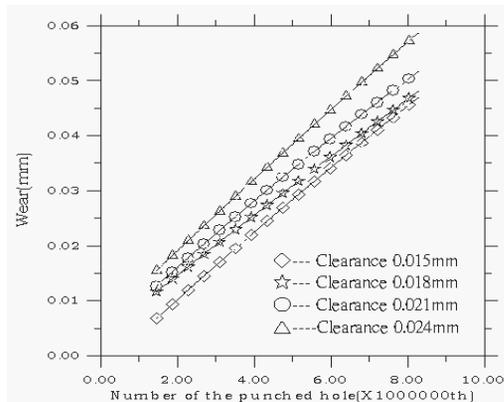


Fig. 13. The relationship between number of the punched hole and wear of punch AO-side

The processing of the punch long side (BO=1.27 mm) is shown in Figure 14, which shows that a punch's wear value is proportional to the total punching times. Clearance size, however, is not proportional to the wear value. This indicates that proper clearance and punching times can help to reduce the wear of punch and to get longer punch's life.

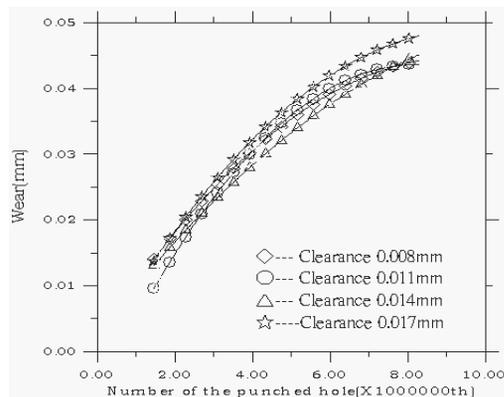


Fig. 14. The relationship between number of the punched hole and wear of punch BO-side

As shown in Figures 15 through 16, most dies wear of AO-side and BO-side are proportional to punching times, except for clearance versus wear value. This indicates that punching die designers should, where applicable, use suitable punching parameters in order to obtain desired wear values.

The simulation is used to illustrate the process of optimizing the clearance parameters. When the weight function  $w_1=1$ . The optimal parameters used in the simulation annealing algorithm are given as follows: the initial temperature  $T_s=100^\circ\text{C}$ , the final temperature  $T_e=0.0001^\circ\text{C}$  the decaying ratio  $C_T=0.98$ , the Boltzmann constant  $k_s=0.00667$ . The upper bound of micro-punch system parameter is

set to clearance=0.024 mm, punching times= $8.27 \times 10^6$ , and the lower bound of micro-punch system parameter is set to clearance=0.015 mm, punching times= $1.458 \times 10^6$ .

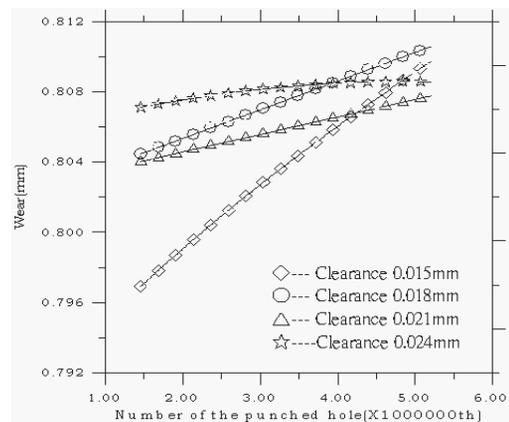


Fig. 15. The relationship between number of the punched hole and wear of die AO-side

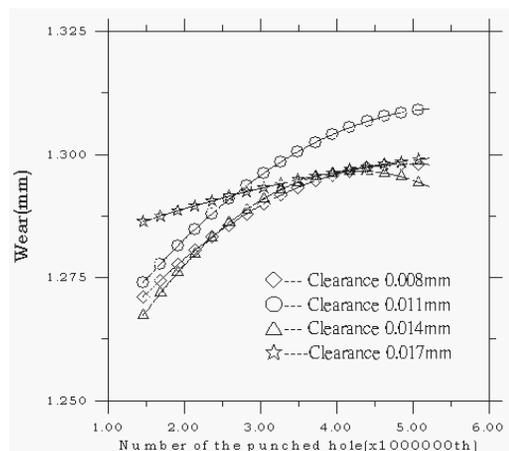


Fig. 16. The relationship between number of the punched hole and wear of die AO-side

The simulated annealing is used for finding the optimal micro-punch system parameters as shown in Table 7. This set of parameters will assure the minimum wear, from the simulated annealing equation, when the punching times in AO-Side of punch is set to  $8 \times 10^6$ , the corresponding clearance has minimum wear. When the parameter of clearance is 0.017 mm, the minimum wear is 0.05355 mm as shown in Fig. 17. Based upon the results of this paper, it has been clearly shown that the optimal punching parameter for micro punching die can be systematically obtained through this approach.

To further verify the results of the micro-punch process as shown in Table 7. The final results were compared with another corresponding experiment data. Based upon the results of this paper, the SA predicted wear comparing with the actual wear of experimental data for this optimized punching process; the error is about 7.6 %

Table 7.  
The error comparison between SA method and experimental data

Item	SA method Punching times	SA method Clearance (mm)	SA method Wear	Experimental data Wear (mm)	Error (%)
Value	$8 \times 10^6$	0.017	0.05355	0.058	7.6

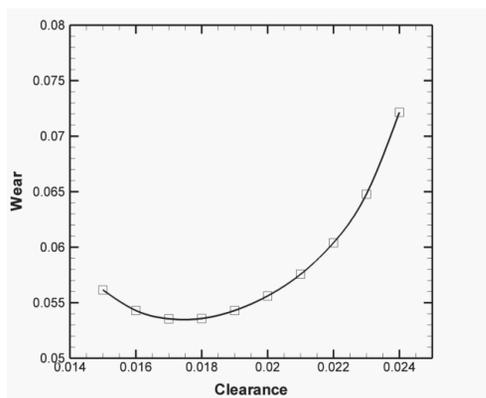


Fig. 17. The relationship between clearance and wear of punch AO-side

## 8. Conclusions

The clearance is a very important parameter in both product quality and the service life of dies. A bigger clearance is positively related to longer service life, while smaller clearance is related to higher product quality, but with shorter life. A good clearance design can not only increase the accuracy of products, but also reduce the burr of products. Therefore, the wear of punch and die can be reduced greatly and the life expectancy of punching dies will be increased.

This study utilizes an Image Vision System to measure the burrs of composite and uses tool microscope to inspect the wears of punch and die in order to estimate which condition is better for micro punching dies. The relational model was established between input parameters and outputs via an adductive network. This can help to anticipate the wear size under any clearance, and contributes to the design and application in the future. The simulated annealing (SA) were used to search for the optimal punching conditions of micro-punching die. The aim is to gain high levels of productivity and to reach a suitable accuracy that meets the required conditions.

The predicted value of wear through adductive network is very close to actual experimental value, with an error of about 8%. Engineers are able to estimate the wear of punches and dies

without any punching experiments or complicated polynomial calculation. Worn punches and dies indicate the end of service life, allowing engineers to replace them before they crack, thus increasing production efficiency.

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